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Short communication

A predictive model to reflect the final stage of spark plasma sintering of submicronic $\alpha$-alumina

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A B S T R A C T

The grain growth/densification interaction is known to strongly decrease the shrinkage rate during the final stages of sintering. This phenomenon was studied for $\alpha$-alumina to provide more accurate sintering models for ceramics. Isothermal interrupted experiments were conducted to identify the parameters of the grain growth law for the model.

Keywords:
Spark plasma sintering
Modeling
Grain growth
Densification

In both pressureless and pressurized sintering processes, like Hot Pressing (HP) and Spark Plasma Sintering (SPS), the grain size is known to have a strong influence on the final stage of sintering. According to Rahaman [1], the attainment of high relative density requires minimization of the grain growth phenomenon. For example, transparent alumina ceramics (porosity lower than 0.1%) were obtained at low temperature or low heating rate [2,3], which allows densification without grain growth. These results can be explained considering the grain size dependence of the diffusion creep mechanisms, Nabarro-Herring (lattice diffusion) [4,5] and Coble (grain boundary diffusion) [6]. In both of them, the displacement is due to atomic motion over varying distances depending on the grain size. The larger the grain, the lower the creep rate, because the atomic diffusion distances increase. Thus, in both lattice and grain boundary diffusion creep, the grain size term appears in the denominator of the creep rate equation:

$$\dot{\epsilon}_c = \frac{CD\sigma^n}{G^{m}RT}$$

(1)

where $\dot{\epsilon}_c$ is the creep rate, $C$ a constant, $\sigma$ the stress, $D$ the diffusion coefficient, $k$ the Boltzmann constant, $G$ the grain size, $T$ the absolute temperature, $m$ and $n$ the grain size and stress exponent, respectively.

In this expression, the creep law appears to be strongly influenced by the grain size exponent. Nabarro and Herring [4,5] determined, for lattice diffusion creep, a value for the grain size exponent $m=2$. On the other hand, Coble [6] established a grain size exponent $m=3$ for grain boundary diffusion creep. Consequently, the determination of the $m$ exponent allows the identification of the diffusional creep mechanism. Most widespread sintering models are built on porous creep behavior law, such as Olevsky’s sintering model [7,8] for which the creep law is coupled to a grain growth law.

In a previous publication [9] on SPS densification modeling of a pure submicronic $\alpha$-alumina powder, we showed that taking into account the grain growth phenomenon allows correction of the relative density values at the final stage of sintering. We showed that, by inverse analysis, it is possible to determine an approximate parameter for the grain growth law using the experimental data obtained at the final stage of sintering. Thus, using this value, the model obtained appears to be reliable since the final average grain diameter calculated is in good agreement with the experimentally observed one. Moreover, the sintering laws identified in various pressure and heating rate conditions converged to a linear ($n=1$) creep behavior. A result similar to that reported by Langer et al. [10] on the same alumina powder.

The aim of the present work is to determine the parameters of the alumina grain growth law by isothermal interrupted tests and to compare the values obtained to those estimated by reverse analysis of our previous study. The other objective is to discuss the grain growth mechanisms and to study the densification/grain growth interaction during the final stage of sintering in the SPS process.

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The sintering experiments were conducted on the Dr. Sinter 2080 SPS machine (SPS Syntex INC JapanCo. Ltd., Japan) of the Plateforme Nationale CNRS de Frittage Flash located at the Université Toulouse III-Paul Sabatier in Toulouse. For each experiment, 1 g of powder (α-alumina 99.99%, reference TM-DAR, Taimei Chemicals Co. Ltd, median particle size 0.14 µm) was introduced and consolidated within an 8 mm inner diameter graphite die. Each experiment was performed under vacuum (< 10 Pa) with a pulse sequence of 12–2 (12 pulses and 2 dead times, each pulse and dead time having a duration of 3.3 ms). For easy removal of the sample graphite foil (e.g. Papyex from Mersen) was introduced at the sample/die and sample/punch interfaces. The heating rate was 100 K/min. The pressure was kept constant at 100 MPa during the whole cycle. In order to identify all the terms of the grain growth law, isothermal tests were performed at three programmed temperatures (1100 °C, 1200 °C and 1300 °C) and with different dwell times (0, 1, 5 and 15 min). The real temperature of the sample was determined in other experiments, performed in similar conditions, with a sacrificial thermocouple located in the powder bed. An empiric function obtained by calibrating the two temperatures at the beginning of the sintering cycle was used to extrapolate the temperature of the dwell to respectively 1305, 1439 and 1575 °C which is due to the presence of the small grains.

The analytic Olevsky’s sintering model [7,8] for uni-axial die compaction can be summarized by Eq. (2):

\[
\frac{\rho}{\rho^0} = \left( K(T, G) \left( \frac{\psi}{\phi} \right)^{1 - \frac{2}{n}} \left( \rho^0 \right)^{\frac{1}{n}} \right)^{\frac{1}{n}}
\]

(2)

where \( \rho \) is the densification rate, \( \rho^0 \) is the relative density, \( \sigma_t \) the applied stress, \( \phi \) and \( \psi \) the shear and bulk moduli, \( K(T,G) \) the creep consistency factor depending on the grain size \( G \) and the temperature \( T \), and the stress exponent \( n \).

Based on our previous work [9] the expression of the consistency factor is:

\[
K(T, G) = \left( \frac{G}{G_0} \right)^{2} \left( \frac{1}{T} \right)^{n} \exp \left( \frac{Q}{nRT} \right)
\]

(3)

Where \( G_0 \) is the initial grain diameter, \( A_0 \) a constant of 0.873 KPa \( \cdot \) s \( ^{-1} \), \( Q \) is the activation energy of 179 kJ/mol and \( n \) the stress exponent equal to 1 [9].

The grain growth law mainly depends on the temperature [1] but may also depends on both the applied pressure \( P \) [15–17] and the relative density \( \rho \) [18]. As we will see later, the grain growth model considered, which does not take into account any pressure or porosity dependence, gives good agreement with experiment, therefore in our experimental domain these dependences \( P \) and \( \rho \) can be ignored. In the present study, expression (4) [19,20]

![Fig. 1. FESEM images of the fracture surfaces of the materials sintered at different temperatures and dwell times.](image)
considered for the grain growth rate ($G$) is only temperature dependent:

$$G = k_0 \exp \left( \frac{-Q_g}{RT} \right) \frac{1}{G^m}$$

where $k_0$ is a constant, $Q_g$ the grain growth activation energy and $R$ the gas constant.

Eq. (4) can be transformed into its logarithmic form (Eq. (5)):

$$\ln(G) = \ln(k_0) - \frac{Q_g}{R} \left( \frac{1}{T} - m \ln(G) \right)$$

at constant temperature the following term of Eq. (5) is a constant:

$$\text{Cst} = \ln(k_0) - \frac{Q_g}{R} \frac{1}{T}$$

As there is not enough available data in the grain growth curve to determine $G$ we have considered a fit (i.e. the interpolation curves reported in Fig. 2).

All of the linear regressions (Fig. 3) give straight lines which, over the experimental domain explored, validate the temperature dependent grain growth model (4).

The slope of the plot of $\ln(G) = f(\ln(G))$ at a given temperature (Fig. 3a) gives an $m$ exponent ranging from 1.89 to 2.12. Considering Eq. (6) and a $m$ value equal to 2, $k_0$ constant and activation energy $Q_g$ were determined (Fig. 3b) and are equal to $5.53 \times 10^{-4} \text{ m}^2/\text{s}$ and $530 \text{ kJ/mol}$, respectively.

For pure materials undergoing normal grain growth, an $m$ value equal to 2 corresponds to a grain boundary control mechanism [21]. The grain growth activation energy of $530 \text{ kJ/mol}$ is in good agreement with that ($520 \text{ kJ/mol}$) determined in previous works by calibration on the final stage of sintering [9]. Olevsky et al. [7] identified a higher grain growth activation energy ($570 \text{ kJ/mol}$) for submicron $\alpha$-alumina probably because of the larger initial grain size of the powder used ($0.38 \mu\text{m}$ vs $0.14 \mu\text{m}$).

To highlight the effect of grain growth on sintering, the grain growth law parameters were used to model previously published sintering data at $1400^\circ \text{C}$ [9]. The result is reported in Fig. 4. The green curve converging at the end of the sintering to a full

<table>
<thead>
<tr>
<th>Dwell temperature ($^\circ \text{C}$)</th>
<th>Dwell time (s)</th>
<th>Average grain size ($\mu\text{m}$)</th>
<th>Standard deviation ($\mu\text{m}$)</th>
<th>Relative density ($\pm 0.5%$)</th>
</tr>
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<tbody>
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<td>0.31</td>
<td>0.08</td>
<td>94.8</td>
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<tr>
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<td>0.11</td>
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<td>0.29</td>
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</tr>
<tr>
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</tbody>
</table>

Fig. 2. Model/experimental isothermal plot of grain size versus time.

Fig. 3. Grain growth model identification a) determination of the $m$ exponent (b) $k_0$ constant and $Q_g$ determination.

Fig. 4. Sintering model with and without grain growth (heating rate 100 K/min, 8 mm diameter sample [9]). (For interpretation of the references to color in this figure, the reader is referred to the web version of this article.).
densification is the one given by the sintering model (Eq. (2)) without taking into account the grain growth law. The blue curve giving a full description of the evolution of the relative density during the final stages of sintering was obtained using the complete sintering model ((Eqs. (2) and (4)) with the grain growth effect.

In conclusion, the grain growth law parameters of a pure submicron α-alumina were determined using isothermal treatments at three temperatures. In the experimental domain considered, the grain growth mechanism suggested by the m exponent is a grain boundary control mechanism. Introducing the parameters obtained in a mechanical model of the sintering process enabled a good description of the relative density curve and in particular of the non-attainment of full densification at the end of the cycle.

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References